

LAMINAR FLOW TECHNOLOGY – THE AIRBUS VIEW

Heinz Hansen
Airbus, Germany

Keywords: *laminar flow; structure concept; surface requirements; flight demonstration*

Abstract

Research in laminar flow has a long tradition and a lot of work has been performed by research organisation and aircraft manufacturers around the world. With a few exceptions (glider aircraft, general aviation or small business aircraft) this technology did not find its way to real industrial application for commercial large transport aircraft.

Increasing fuel costs and the need for reduction of the environmental impact of airline operation has lead to a new effort to apply this technology for the next generation of aircraft.

A key element for application of laminar flow technology is a structure concept that fulfils the high aerodynamic surface requirements and what can be manufactured at acceptable costs and production rates at the same time. The paper will explain the experience Airbus has collected within previous research projects on that topic and the steps which have and will be performed to introduce this technology in future for transport aircraft.

1 Introduction

Together with new engine technologies laminar flow has the highest potential to reduce the fuel burn. The main reason why this technology has not been introduced so far for large transport aircraft is the fact that for this category of aircraft with very high Reynolds numbers extreme requirements for surface quality have to be fulfilled. Two different types of laminar flow have to be considered: natural laminar flow (NLF) by specific shaping of the wing airfoils and hybrid laminar flow control (HLFC) as a

combination of shaping and active means (e.g. suction) to increase boundary layer stability.

Both technologies are applicable for different conditions: NLF is more related to smaller, low sweep wings and HLFC can offer some advantage for a large aircraft flying at high Ma numbers. The surface requirements and therefore the structural concepts are different but there are a lot of common issues for both concepts which will be explained in more detail in this paper.

2 Previous Airbus Activities on Laminar Flow Research

Laminar flow research has a long tradition all over the world [1, 2, 3, 4, 5, 6, 8]. Airbus together with research partners in Europe has started a lot of activities around NLF and HLFC in the 90ties. A major objective at that time was to establish a toolset for prediction of laminar extent on wings under realistic flight conditions.

The application of linear stability with determination of limiting amplification factors (N factor) in the relevant environment (wind tunnel; free flight) could be identified as a valuable tool for the aerodynamic design of laminar surfaces [8, 9, 11].

Several major design steps (VFW614 NLF glove flight test; F100NLF glove on upper and lower side flight test; large HLFC wind tunnel models; A320 HLFC fin flight test) could demonstrate the increasing aerodynamic design capability. An overview about the different activities and projects performed together with several partners is given on Fig. 1 and some of the references for these activities can be found in [7, 9, 10, 12]. Major flight or ground tests are

indicated in blue, major wind tunnel tests in red and tool development work in green.

A major result of these tests was not only the improved aerodynamic design and measurement capability but at the same time first indications about the need for high surface quality. An interesting example for that is given on Fig. 2 and in [7]. During the first flight tests with a laminar glove on the F100 wing the extent of laminar flow was poor. Detailed analysis of the manufactured surface quality showed that some kind of waviness was the origin of the problem. After re-work of the surface a laminar extent as expected could be obtained. Very useful information could be derived from this exercise and underlined that surface quality is the key for introduction of such a technology.

3 Major Activities and Strategy for Application of Laminar Flow

Within the next chapters the three major elements for introduction of laminar flow technology for large aircraft application will be described.

3.1 Aerodynamics

As explained in the previous chapter a useful and validated toolset for aerodynamic design could be build up within Airbus. There is a high confidence that we are able to predict laminar flow extent with sufficient accuracy. Due to measurements in several wind tunnel facilities and the N-factor calibration for these tunnels (e.g. ONERA S1, ETW) both computational and wind tunnel tools can be applied for performance predictions.

Two new streams have got more focus now: 1. Find best compromise on aircraft level considering mainly implications on surface quality and complexity/weight and costs. 2. Improve knowledge about surface requirements to give as precisely as possible constraints for NLF and HLFC structure concepts. This last point will have a significant effect on manufacturing costs and time. One example of that activity is given on Fig. 3. Here a very specific cryogenic wind tunnel test has been

performed to get information about allowable step heights under realist conditions. Realistic means here: comparable boundary layer stability situation very similar to a real laminar wing application and simulation at nearly flight Reynolds numbers. With this test it could be demonstrated that the effect of steps is strongly dependent on the stability situation and that by proper design, surface requirements can be relaxed.

3.2 Structure Concepts

As already underlined with the F100 example in the previous chapters the major focus for introduction of laminar flow technology is on a feasible structure concept. In the past all flight test experiments have been performed with a glove technology on top of the existing wing structure. Such a glove was then hand finished with a lot of effort to get high surface quality.

This is acceptable in a research environment but if this technology has to be applied under typical production standards (high rate, low costs) then a completely new concept has to be developed.

Several surface requirements have to be considered for such a concept:

- No steps or steps with very limited step height
- Reduced waviness (either from manufacturing or deformation under cruise loads)
- Avoidance of any 3D disturbances (by insects or rivet heads)
- Reduced roughness at the leading edge (either from manufacturing or erosion under operational conditions)

This long list shows that this is a real challenge if on top of all this additional constraints from manufacturing / assembly/ repair time and costs and weight limitations have to be considered. A typical example of waviness effect at cruise conditions is given on Fig. 4 left. Here the effect of local deformation by air loads is shown. Such a tiny waviness in the order of less than 1 millimeter can create premature transition and therefore means have to be found to reduce those effects. By manufacturing additional effects will come on

top of these deformation effects. A typical example is given on Fig 4 right for a CFRP wing box panel. Around each stringer a waviness is detected by a very precise surface measurement technique. This waviness is caused by spring in effects around stringers or other substructure and strongly dependent on design features of stringer feet, thickness and manufacturing process and sequence. Detailed studies have been performed at Airbus to quantify and control these effects as precisely as possible for a laminar wing outer surface.

A very important decision is the wing concept itself. Several solutions are possible but each has his own pros and cons. A continuous surface with any separation between wing box and the leading edge part is from an aerodynamic point of view the best, but here repair and integration of systems is a challenge. Another concept with a joint between the box and leading edge offers here some kind of flexibility, but creates a risk of non acceptable steps at the joint. Therefore experiments described in the previous chapter are important to give structure and manufacturing realistic aerodynamic requirements.

A major problem for introduction of laminar flow is the disturbance created by insect debris at the wing leading edge during summer time. Due to the fact that most of these insects can be found during the taxiing, climb or landing phase a very effective way to reduce or avoid insect contamination is to use the high lift leading edge elements as an insect shielding device. Several tests have been performed to demonstrate this [13]. Fig. 5 shows such a pretest performed by DLR on Do228 test aircraft with a Krueger element used as insect shield. A nearly 100% success could be demonstrated. Within this test campaign it could also be demonstrated that a combination of a perforated surface (used for HLFC) can be combined with cleaning fluid to reduce contamination by insect.

Another possibility is to develop specific mechanical cleaning devices. This cleaning process can be supported with coatings which can offer easy to clean properties. The objective here is to develop coatings which are erosion

resistant and can be combined with other functions like ice adherence reduction.

Due to the specific pressure distribution needed for laminar flow a very narrow leading edge is created. This is causing several problems for the integration of high lift and other systems. Especially if this is combined with a suction system for hybrid laminar flow this can create a real challenge. At Airbus therefore a specific kinematics concept for a Krueger system has been developed which fits to the space available for a laminar wing and which can provide at the same time a correct setting of the Krueger for the insect shielding function.

3.3 Demonstration

Before a decision can be taken to go for such a risky technology a sufficient high readiness level has to be reached. Therefore demonstration at realistic conditions is a clear request. For the aerodynamic design of a laminar flow concept the Reynolds number is the key parameter. This Reynolds number should be as near as possible to the flight conditions. This can only be reached by testing directly at flight with the real geometry or by testing in wind tunnels at smaller scale but with specific features to reach flight Reynolds numbers. The cryogenic test facility ETW (European Transonic Windtunnel) offers here the unique possibility to combine high pressure with extreme low temperature to reach flight Reynolds numbers comparable to flight. Fig.6 shows an example for such a laminar flow experiments in the frame of the European research project TELFONA [14]. As described in chapter 2 a calibration for such a tunnel is needed, to translate results to flight. This was done by a specific pre-test.

The size of models in a wind tunnel is limited and therefore any simulation of structure features is a challenge. Especially if the objective is to check a complete structure concept and its practicality, a large scale experiment is needed.

Within the large European research project Smart Fixed Wing Aircraft (SFWA) it was

therefore planned to go for a flight test experiment for demonstration of laminar technology. The A340-300 flight test aircraft was selected and a concept developed to exchange the existing outer wing of this aircraft with a new wing with a laminar aero design. In contrast to all previous experiments it is planned not to use an existing structure but to build a complete new wing structure which is as near as possible to a production standard required for a laminar wing structure concept. Fig.7 shows a sketch of this arrangement. Both wings are exchanged. This offers the possibility to check different structure concepts at same nominal outer shape.

Three major objectives for such a flight test can be given as follow:

- demonstrate in flight that aero design for a laminar wing is feasible and can be achieved with the tools developed
- fly a wing structure concept that can provide sufficient surface quality to enable laminar flow with expected extent and which is representative for a possible laminar wing structure
- demonstrate this in an environment which is relevant for a laminar wing application

A major constraint is to realise all this for a boundary layer stability situation which is typical for a new aircraft application (Ma, Re range and pressure distribution)

By using an existing aircraft as carrier for such an experiment several constraints are introduced especially for the structure concept. Therefore in parallel some critical structure features will be tested on ground with large structure demonstrators. All knowledge collected by these tests will be introduced in simulation of specific surface imperfections on the flight demonstrator. Specific measurement technique is under development for detailed measurement of local surface deformation in flight. This will offer the possibility to correlate any change in laminar extent to the surface quality conditions and to derive clear guidelines for structure design and manufacturing.

4 Outlook

Laminar flow technology is a very promising element for reducing fuel burn. For application of such a technology a structural concept has to be developed which can provide high surface quality over the complete lifetime of an aircraft. Such a structure concept has to consider from the beginning production cost and time to come to a solution which can be sold to airlines. Increasing fuel costs will be a major driver to accelerate the application and to increase airline interest of such a technology.

Close cooperation between the major discipline aerodynamic, structure and manufacturing is needed to find a solution which is the best compromise on aircraft level. Together with several European research organisations and manufacturing partners the flight test demonstrator in SFWA is under preparation and will deliver a major step for introduction of laminar flow for the next generation of aircraft.

References

- [1] W. Tollmien. „Über die Entstehung der Turbulenz“. 1. Mitteilung, Nachr. Ges.Wiss. Göttingen, Math. Phys. Klasse, 1929, pp. 21-44. English translation: NACATM-609, 1931.
- [2] G.B. Schubauer and H.K. Skramstad. „Laminar Boundary-Layer Oscillations Stability of Laminar Flow“. J. Aero. Sciences, Vol. 14, No. 2, 1947, pp. 69-78.
- [3] W. Pfenninger. “Some Results from the X21 Program. Part I: Flow Phenomena at the Leading Edge of Swept Wings”. Recent Developments in Boundary Layer Research. Part IV. AGARDograf 97, May 1965.
- [4] D.I.A. Poll. “Some Observations of the Transition Process on the Windward Face of a Long Yawed Cylinder”. J. Fluid Mech. (1985), Vol. 150, pp. 329-356.
- [5] Braslow, A.L. “A History of Suction-Type Laminar-Flow Control with Emphasis on Flight Research”. NASA History Division, *Monographs in Aerospace History No. 13*, Washington DC, 1999.
- [6] Redeker, G., Horstmann, K. H., Koester, H., Thiede, P., and Szodruch, J., “Design of Natural Laminar Flow Glove on a Transport Aircraft,” AIAA Paper 90-3043-CP, Aug. 1990.
- [7] N. Voogt. “Flight Testing of a Fokker 100 Aircraft with Laminar Flow Glove,” Proceedings of the Second European Forum on Laminar Flow

Technology, AAAF Rept., AAAF, Paris, France, 1996, pp. 2-3-2-14.

[8] D. Arnal. "Boundary Layer Transition. Predictions Based on Linear Theory". In Special Course on Progress in Transition Modelling, AGARD Report 793, April 1994.

[9] G. Schrauf. "Large-Scale Laminar-Flow Tests Evaluated with Linear Stability Theory". AIAA Journal of Aircraft, Vol. 41, No. 2, 2004, pp. 224 - 230.

[10] Henke, R., "The Airbus A320 HLF Fin Programme," Nouvelle Revue d'Aeronautique et d'Astronautique, Vol. 209, No. 2, pp. 53-55.

[11] Schrauf, G., Bieler, H., and Thiede, P., "Transition Prediction—The Deutsche Airbus View". First European Forum on Laminar Flow Technology, DGLR Rept. 92-06, DGLR, Bonn, Germany, 1992, pp. 73-82.

[12] Schrauf, G., "Status and perspectives of laminar flow", The Aeronautical Journal, Vol. 109, No. 1102, December 2005, pp. 539-644

[13] K. H. Horstmann, J. Meyer, C. H. Rohardt, S. Kommallein. „HYLTEC Laminar Flow Systems Flight Tests: Flight Testing of Anti-Icing and Anti-Contamination Systems on the DLR DO228 Test Vehicle". CEAS Confrence, London, 10-12 June, 2003

[14] Schrauf, G., Horstmann, K. H., Streit, T., Perraud, J. and Donelli, R., "The Telfona Pathfinder Wing for the Calibration of the ETW Wind Tunnel" KATnet II Conference on Key Aerodynamic Technologies, 12-14 May, Bremen, 2009

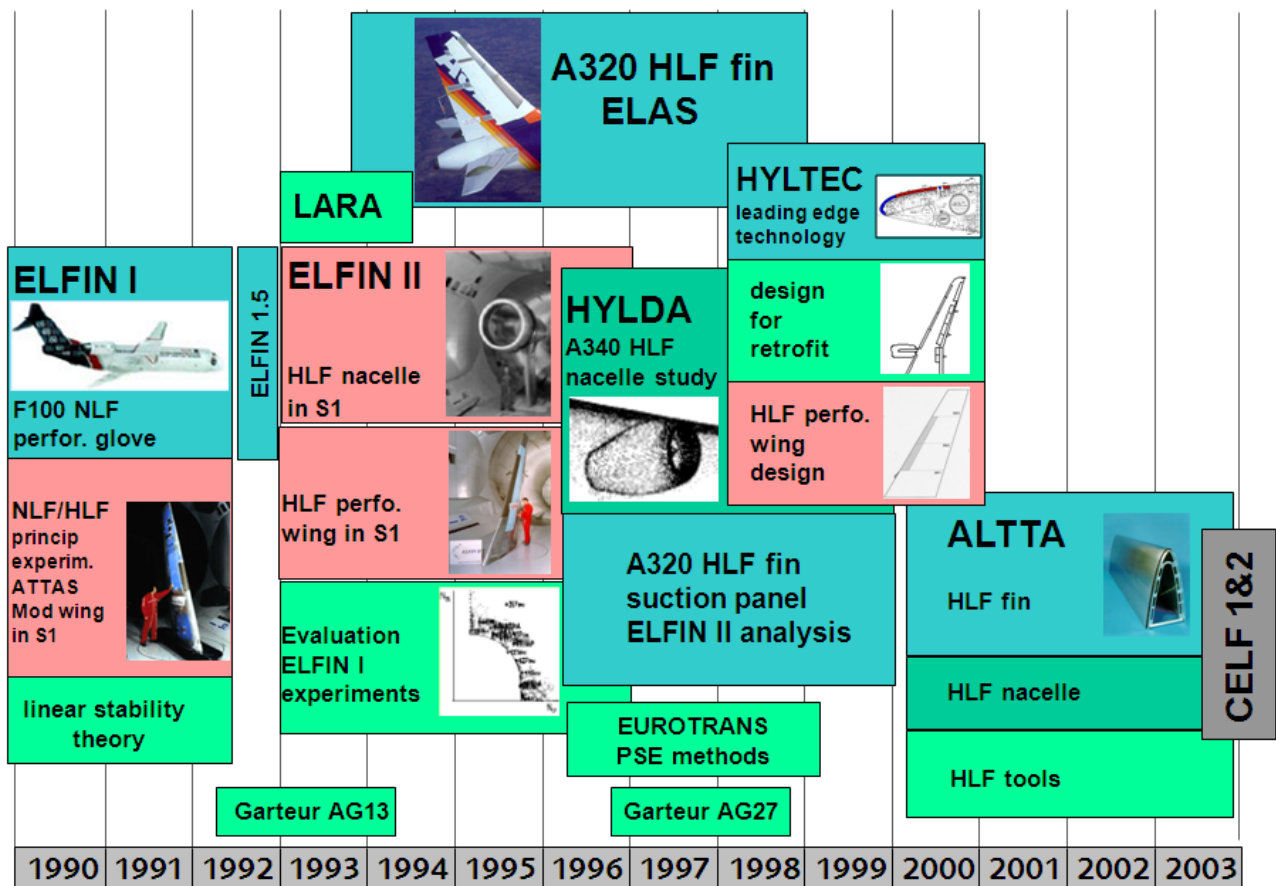


Fig. 1: Overview about Airbus activities for laminar flow

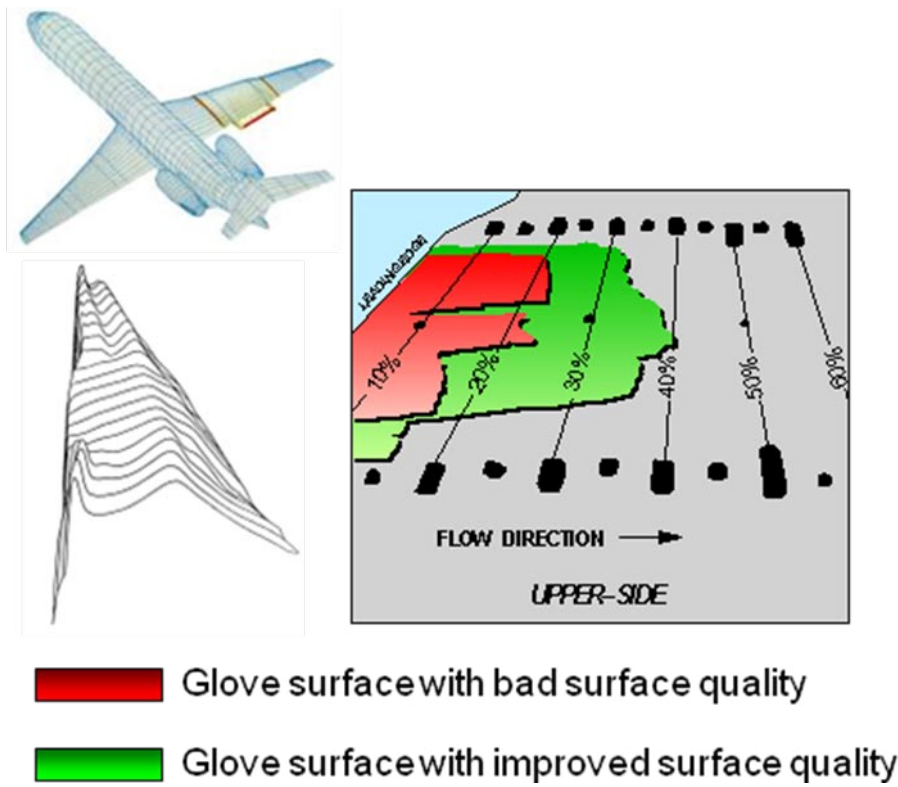


Fig. 2: Effect of repair of F100 flight test glove on extent of laminar flow

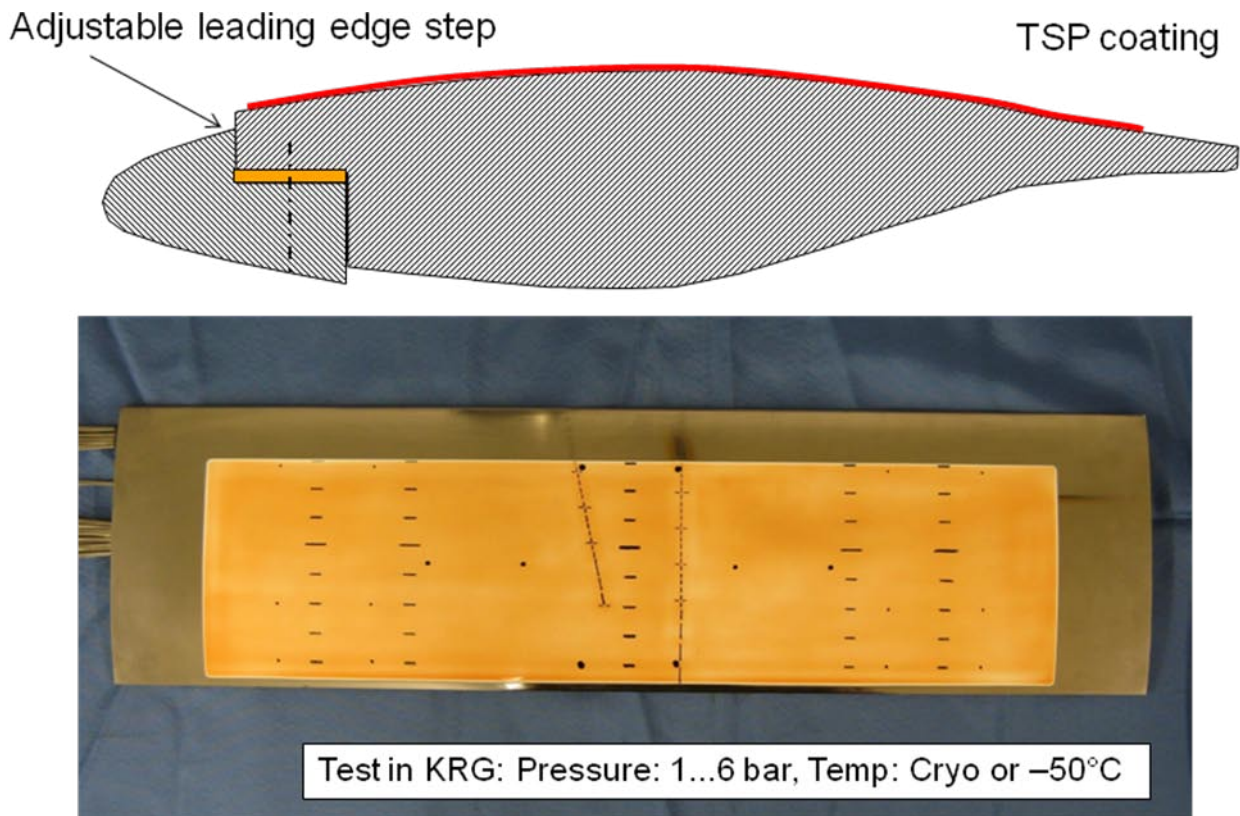


Fig. 3: KRG Wind tunnel model for testing of allowable step height at different Reynolds number

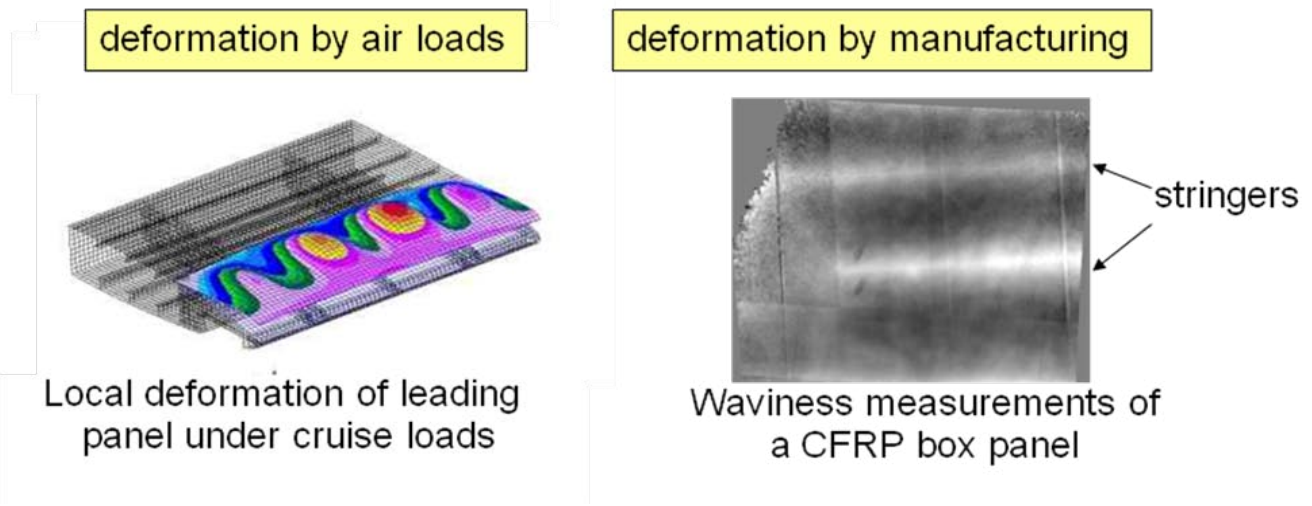


Fig. 4: Examples of waviness caused by loads and manufacturing

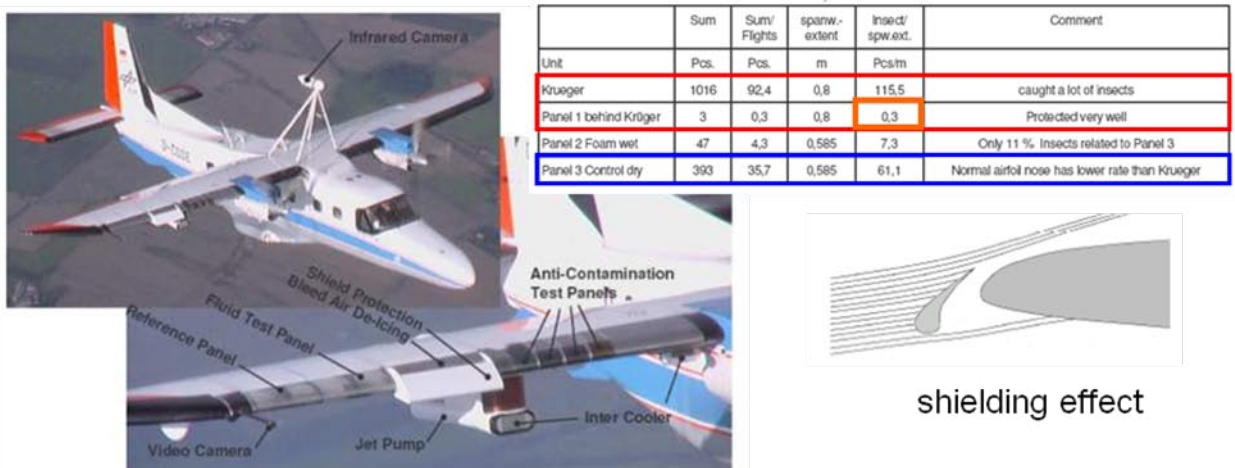


Fig. 5: Flight tests with DLR Do228 and Krueger element as insect shielding device



Pathfinder model for N-factor calibration



Performance model for laminar wing studies

Fig. 6: ETW Wind tunnel models for N-Factor calibration and performance testing at flight Reynolds numbers

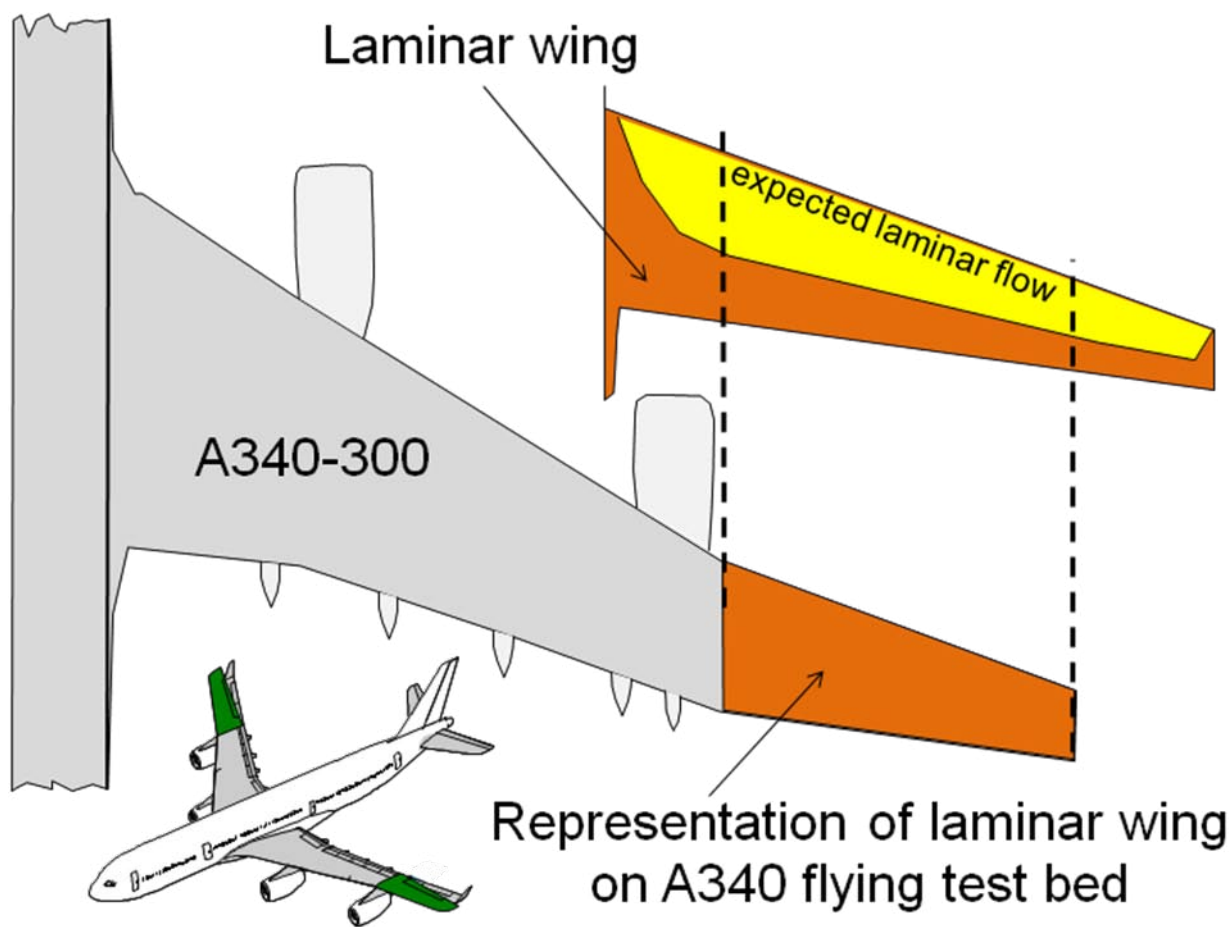


Fig. 7: A340 Flight test demonstration planned in the frame of the European research project SFWA

Contact Author Email Address:
heinz.hansen@airbus.com

Copyright Statement

The authors confirm that they, and/or their company or organization, hold copyright on all of the original material included in this paper. The authors also confirm that they have obtained permission, from the copyright holder of any third party material included in this paper, to publish it as part of their paper. The authors confirm that they give permission, or have obtained permission from the copyright holder of this paper, for the publication and distribution of this paper as part of the ICAS2010 proceedings or as individual off-prints from the proceedings.